

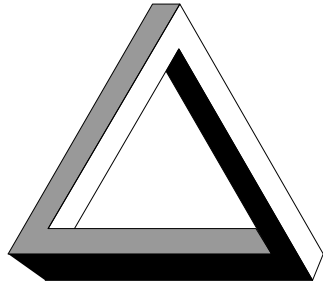
***Difficulties in computing the fundamental  
distortion mode in Coriolis mass flow meters***  
***CLAPDE 2008***

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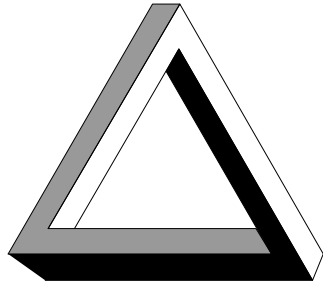
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## ***Focus***

- The Coriolis effect
- Coriolis mass flow meters
- Collaboration and background
- Eigenvalue problem & results



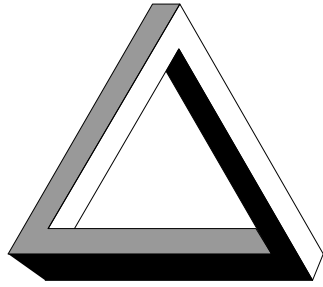
# Coriolis



Gaspard-Gustave de Coriolis (Gustave Coriolis, May 21, 1792 — September 19, 1843) published the paper that described the effect that now bears his name in 1835: *Sur les équations du mouvement relatif des systèmes de corps* (On the equations of relative motion of a system of bodies).

Source:

[en.wikipedia.org/wiki/Gaspard-Gustave\\_Coriolis](https://en.wikipedia.org/wiki/Gaspard-Gustave_Coriolis)



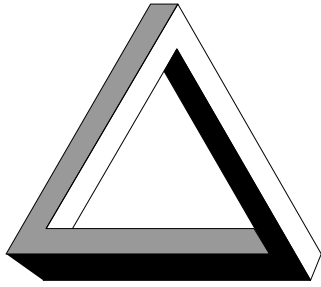
# The Coriolis effect

Imagine rolling a ball radially outward at constant velocity  $V_s$  m/s from the centre of a roundabout/carousel that is rotating at  $\omega$  rad/sec.

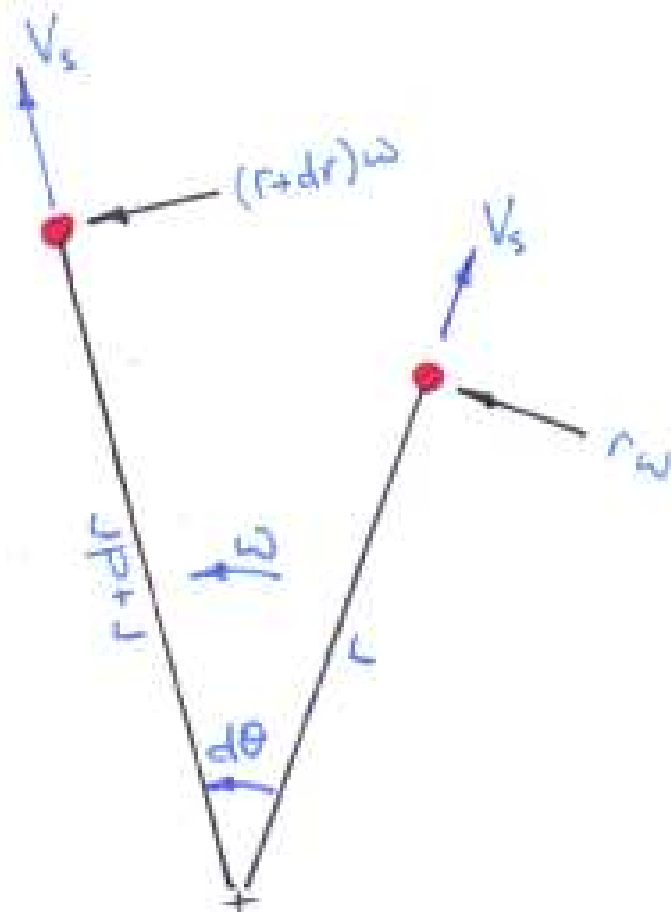
The ball will experience:

- a radial centripetal acceleration
- a tangential Coriolis acceleration

Consider the change in velocity during  $dt$ ...



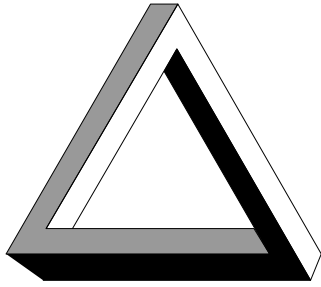
# Derivation I



Sketch the velocity vectors at  $t$

And those at  $t + dt$

Hence obtain accelerations.



# Derivation II

Change in **tangential velocity**

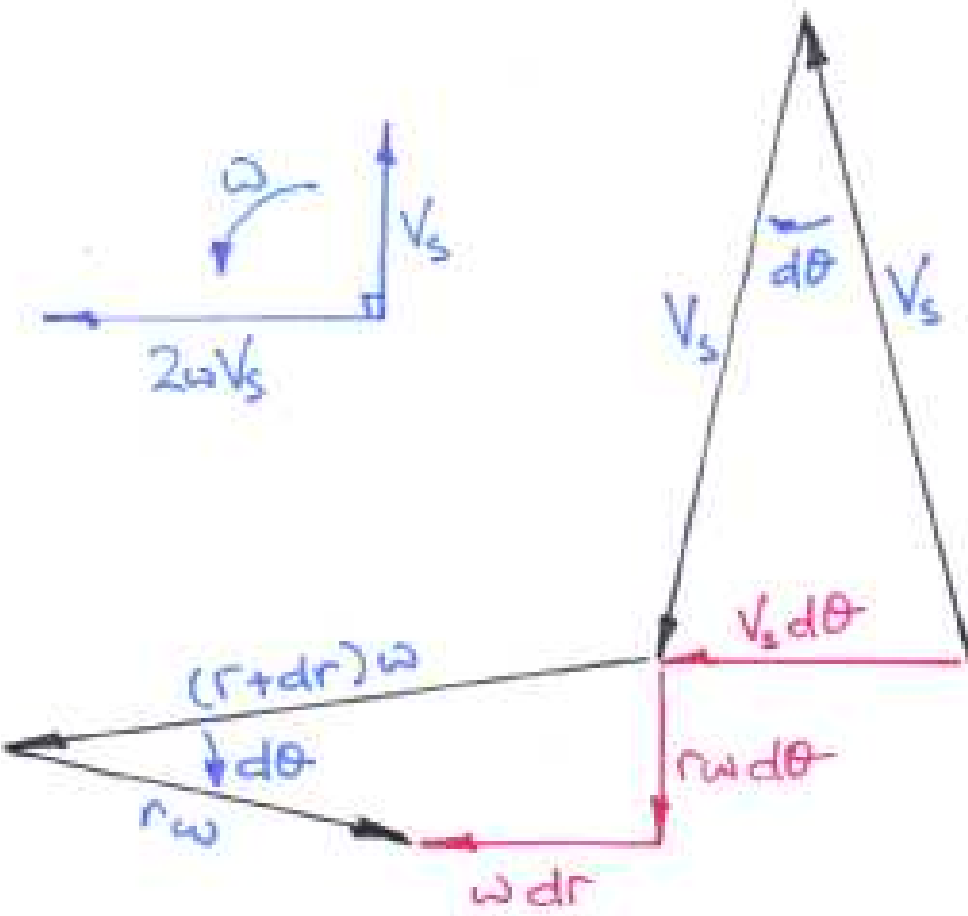
$$V_s d\theta + \omega dr$$

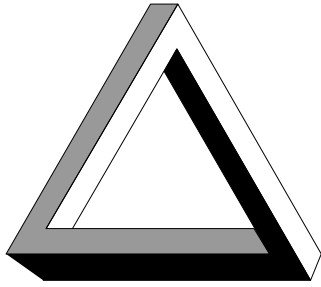
Change in **radial velocity**

$$r\omega d\theta$$

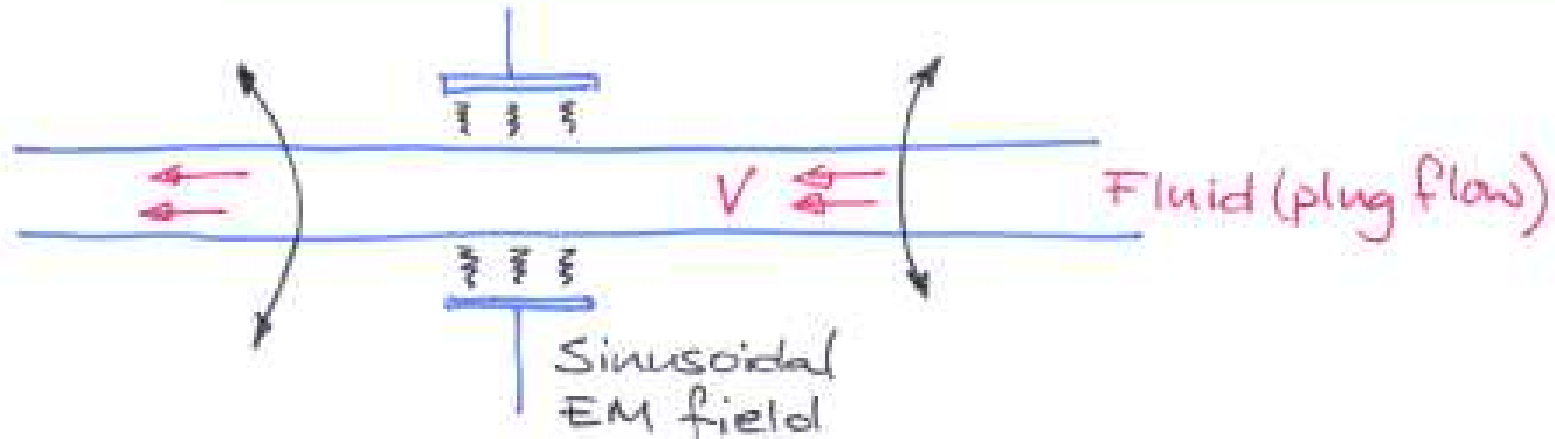
Divide by  $dt$  to get acceleration:

tangential:	$2\omega V_s$	<b>Coriolis</b>
radial:	$r\omega^2$	<b>Centripetal</b>



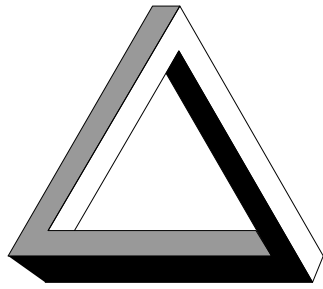


# Pipe meter physics I



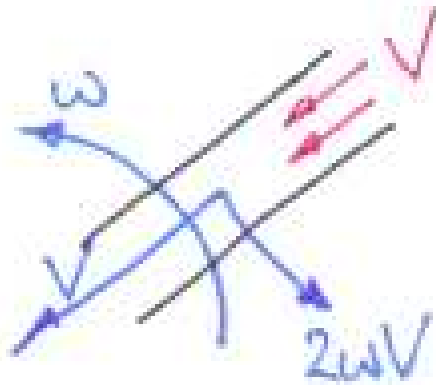
CLAMPED BOUNDARY CONDITIONS

- Metal pipe carries a plug flow of fluid at velocity  $V$ .
- Pipe also vibrated by electromagnetic sine
- Bending theory applies

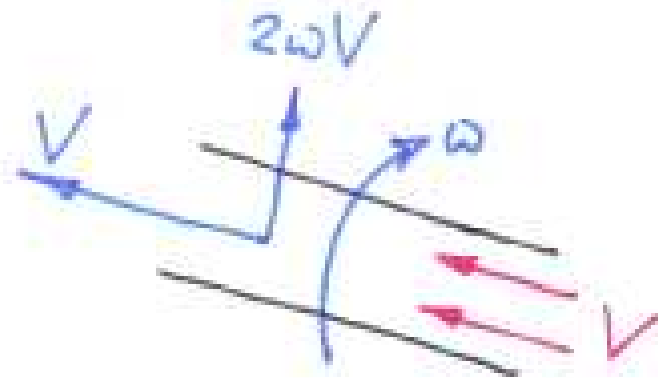


## Pipe meter physics II

LEFT END

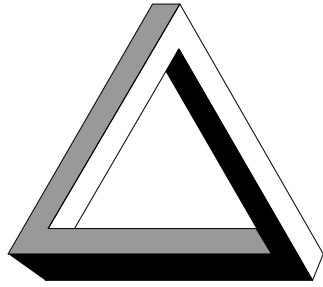


RIGHT END



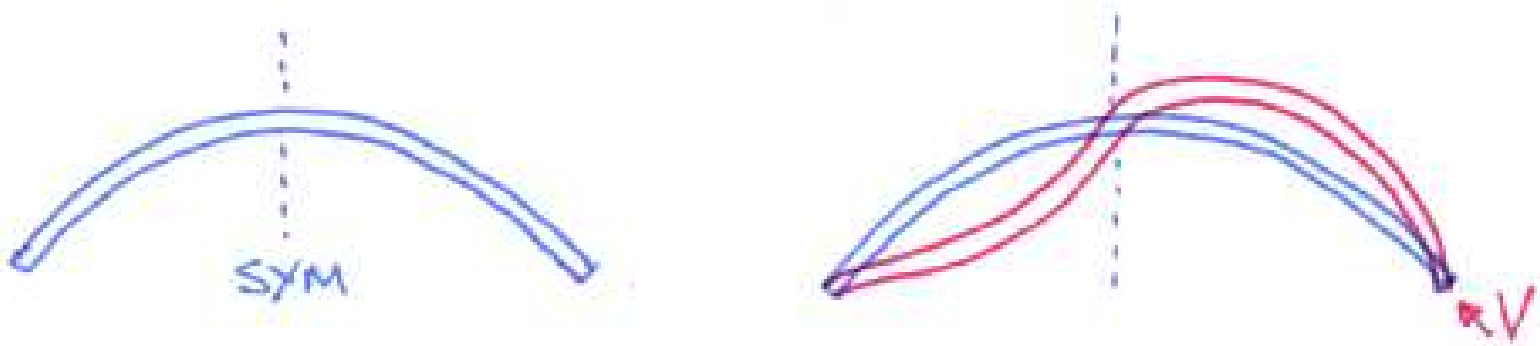
- Right end: fluid particle = ball on roundabout.
- Coriolis acceleration implies force implies deformation.
- Left end: Coriolis force is in opposite direction.



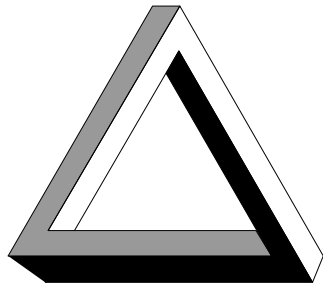


## Pipe meter physics III

No flow on the left, flow at  $V$  m/s on the right:



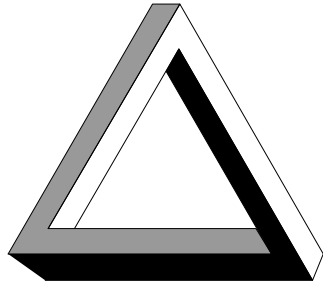
- Overall effect: antisymmetric **Coriolis distortion** superimposed on symmetric bending profile.
- Phase difference at quarter-points **proportional** to **mass flow**



## So what?

Why does this matter?

- Coriolis distortion is an **inertial** effect and is proportional to the **mass** (not **volume**) flow rate.
- Mass flow is measured **directly** not by the **indirect** conversion of volume flow (e.g. bubbles).
- Important for accuracy:
  - Custodial transfers
  - medical drug dosing
- Meters range from over **1 metre** diameter to **micro-machined** (fits on a thumb).

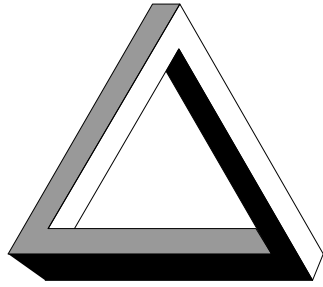


## *Example from wikipedia*

An illustrative example:

- No flow
- With flow

Courtesy [wikipedia](#).



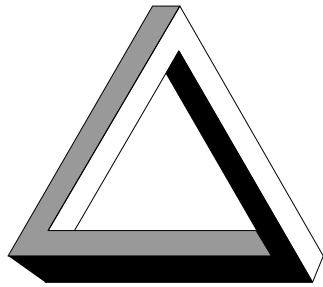
## *The mathematical model*

Incorporating the fluid flow (plug flow) into a Timoshenko beam model leads to,

$$(m_p + m_f) \frac{\partial^2 u}{\partial t^2} + m_f \left[ 2V \frac{\partial^2 u}{\partial x \partial t} + V^2 \frac{\partial^2 u}{\partial x^2} \right] - \kappa G A_p \left( \frac{\partial^2 u}{\partial x^2} - \frac{\partial \theta}{\partial x} \right) = 0,$$

$$(\rho_p I_p + \rho_f I_f) \frac{\partial^2 \theta}{\partial t^2} - E I_p \frac{\partial^2 \theta}{\partial x^2} - \kappa G A_p \left( \frac{\partial u}{\partial x} - \theta \right) = 0,$$

where  $V$  = fluid velocity, and the boundaries are clamped.



Finite element discretization leads to,

$$M \frac{d^2 U}{dt^2} + E \frac{dU}{dt} + AU = 0,$$

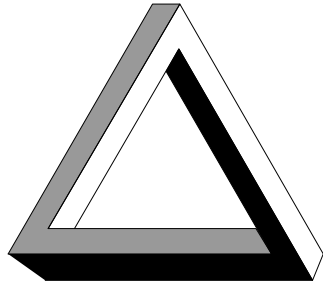
and setting  $U = V e^{i\omega t}$  we get the complex eigenvalue problem,

$$(A + i\omega E - \omega^2 M)V = 0.$$

Here  $E = -E^T$ ,  $M > 0$  and  $A > 0$  (if  $m_f V^2$  is small enough).

It follows that: all  $\omega \in \mathbb{R}$  and if

$$(\omega, V) \text{ is an eigenpair then so is } (\omega, \bar{V}).$$



# *Three solution techniques*

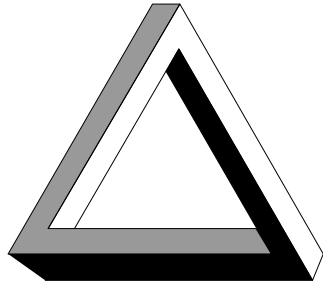
We are looking for the **Coriolis distortion**:

imaginary part of an eigenvector associated with the  
smallest-in-magnitude eigenvalue

Three methods are used:

- Matlab's **polyeig** routine.
- Matlab's **eig** routine.
- **Inverse iteration**.

All with and without shift.

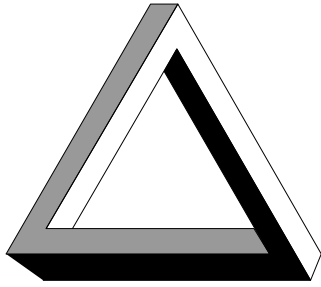


*polyeig* for  $(A + i\omega E - \omega^2 M)V = 0$

The MATLAB fragment

```
[X, e] = polyeig(A, i*E, -M);
```

solves the quadratic eigenvalue problem in terms of a column of eigenvalues,  $e$ , and a matrix of eigenvectors,  $X$ . (Recall that  $A$  and  $M$  are invertible.)



***eig* for  $(A + i\omega E - \omega^2 M)V = 0$**

Set  $W = \omega V$  so that  $-\omega^2 MV = -\omega MW$ . Then:

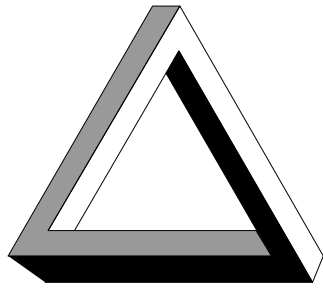
$$\begin{pmatrix} 0 & I \\ M^{-1}A & iM^{-1}E \end{pmatrix} \begin{pmatrix} V \\ W \end{pmatrix} = \omega \begin{pmatrix} V \\ W \end{pmatrix}.$$

Hence:  $BX = XL$ , with  $L$  = diagonal of eigenvalues and  $X$  = eigenvectors. Solve in MATLAB via the fragment,

```
B = [ zeros(N,N) eye(N) ;  
      M\A        i*M\E ];  
[X L] = eig(B);
```

(where  $A$ ,  $E$  and  $M$  are  $N \times N$ ).





## Inverse iteration

Given  $D > 0$  and  $x_0$  the iteration:

- $z_{n+1} = D^{-1}x_n$  for  $n = 0, 1, 2, \dots$
- $x_{n+1} = z_{n+1} \|z_{n+1}\|_{\infty}^{-1}$

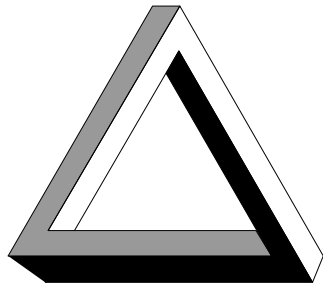
converges to the eigenvector of the eigenvalue of least modulus of  $D$  (if this is well-defined).

For our system this is,

$$W_{n+1} = V_n$$

$$V_{n+1} = A^{-1} (MW_n - iEW_{n+1})$$

and we take  $(1 + 10^{-5}i, 1 + 10^{-5}i, \dots)$  as the initial guess.



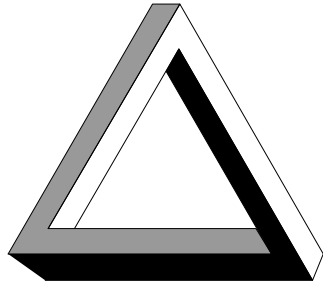
# Summary

These methods were used with and without shift.

The physical constants in the PDEs are 'real life' and correspond to a real straight-tube meter.

Most meters are far more complicated in terms of design and geometry.

Before the numerics here is the background.



## ***Collaboration and background***

Robert Cheesewright (Engineering, Brunel) was getting incorrect eigenvectors from ANSYS.

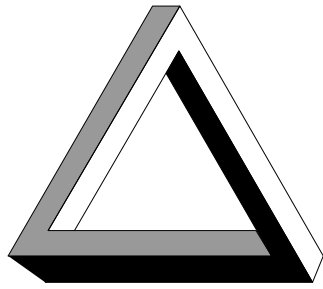
He asked for my help and advice in terms of FEM and 'locking'.

My independent C++ and matlab computations still gave incorrect results...

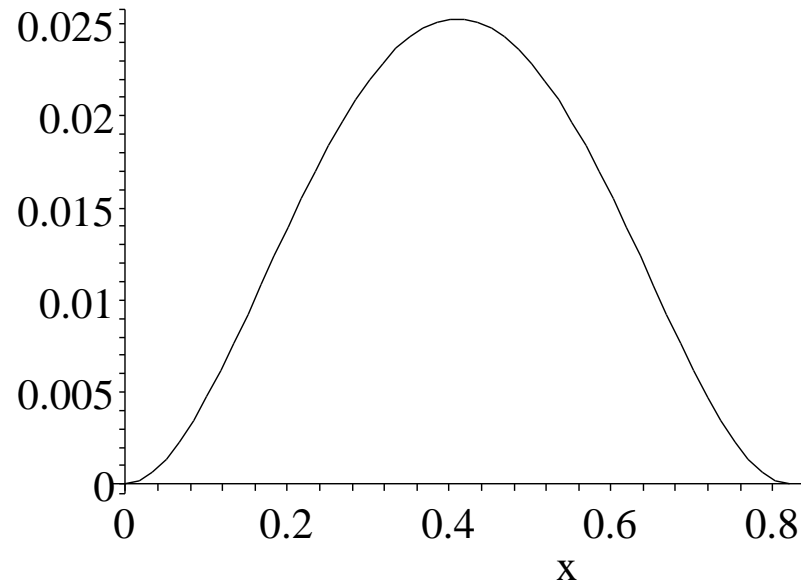
The Timoshenko beam results are shown

The Euler-Bernoulli results are essentially the same

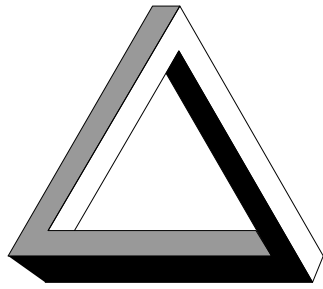
The results for a straight tube meter are...



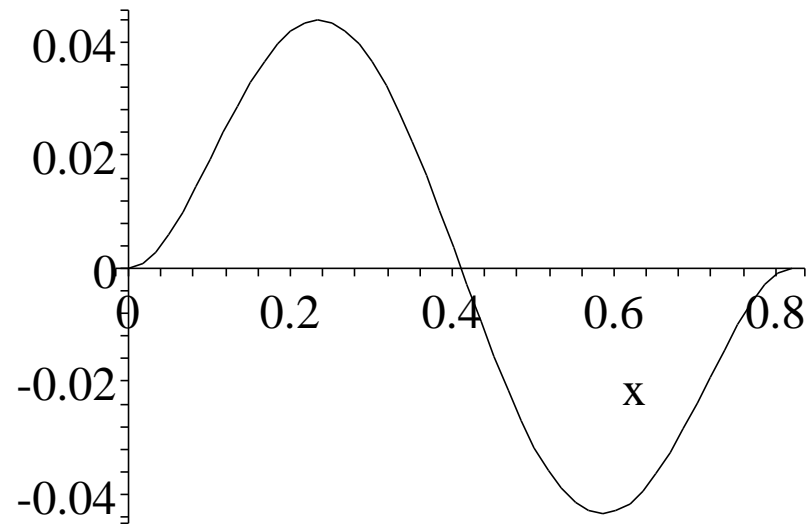
## ***Centrifugal distortion (by analysis)***



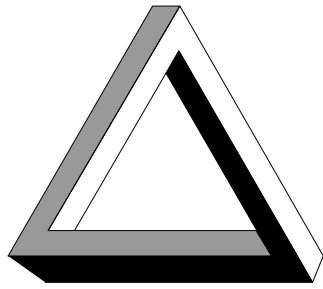
Distortion (in millimetres) due to centrifugal forces as a function of distance (in meters) along the tube, as predicted by analysis.



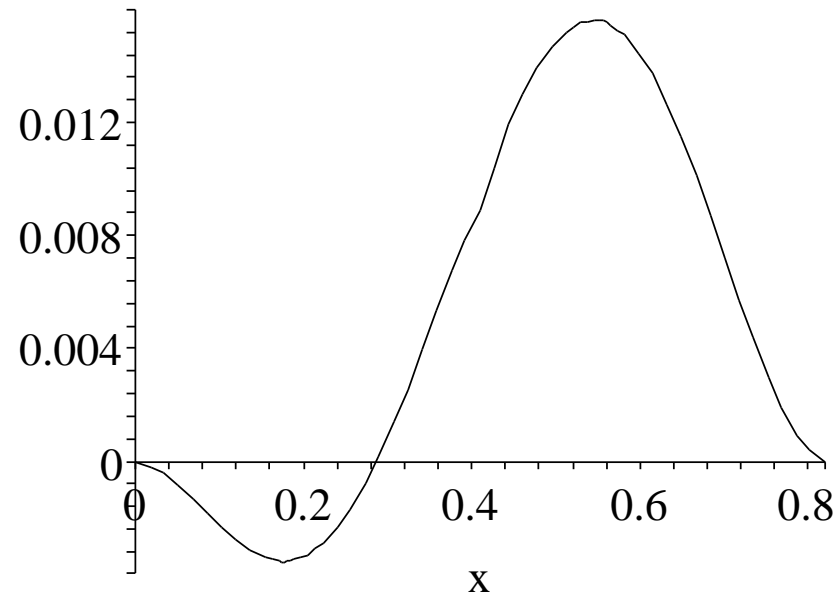
## ***Coriolis distortion (by analysis)***



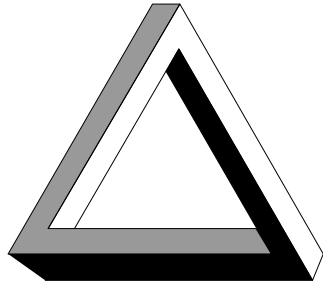
Distortion (in millimetres) due to Coriolis forces as a function of distance (in meters) along the tube, as predicted by analysis.



## Centrifugal distortion (by **ANSYS**)



Distortion due to Coriolis forces as a function of distance along the tube, as predicted by FE modelling using **ANSYS**.

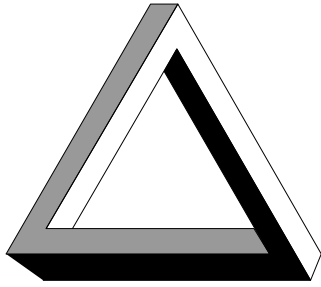


## *My efforts...*

The coriolis distortion is **wrong** and not physical.

My efforts:

- C++ code to generate FE matrices
- Data read by matlab for eigen-computations
- The results were...

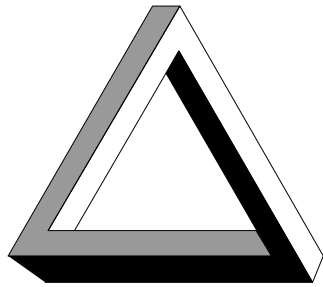


## *Eigenvalues (no shift)*

$N_e$	$ \omega _{\min}$ by technique...		
	1	2	3
16	940.1753	940.1753	$\approx 1 \leftrightarrow 13000$
32	938.9266	938.9266	$\approx 1 \leftrightarrow 13000$
64	938.8359	938.8359	$\approx 1 \leftrightarrow 13000$
128	938.8298	938.8300	$\approx 1 \leftrightarrow 13000$
256	938.8296	938.8296	$\approx 1 \leftrightarrow 13000$

Computed  $|\omega|_{\min}$  for the Timoshenko beam (quadratic elements) with no shift,  $p = 0$ .

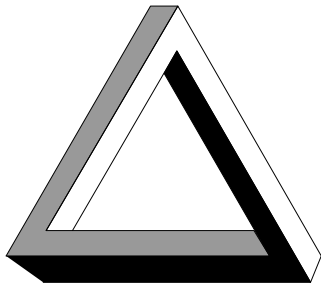




## *Eigenvalues (with shift)*

$N_e$	$ \omega _{\min}$ by technique...		
	1	2	3
16	940.1753	940.1753	940.1753
32	938.9266	938.9266	938.9266
64	938.8359	938.8359	938.8359
128	938.8300	938.8300	938.8300
256	938.8296	938.8296	938.8296

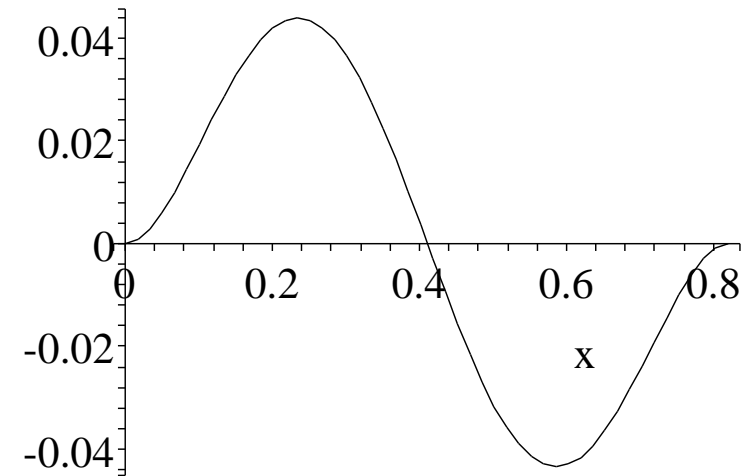
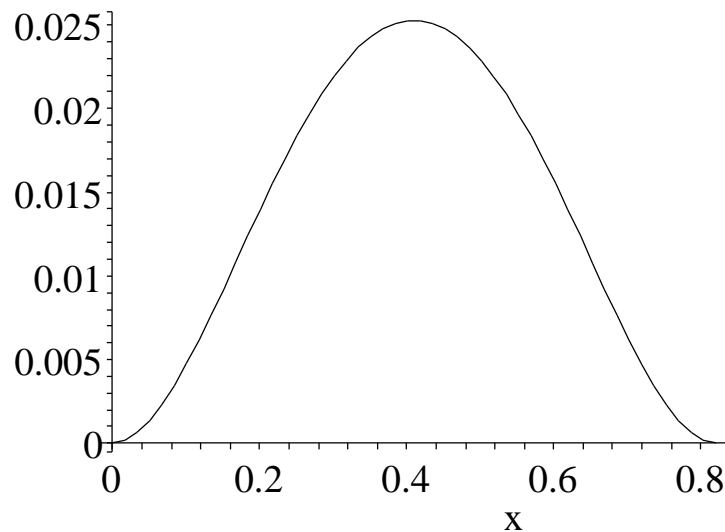
Computed  $|\omega|_{\min}$  for the Timoshenko beam (quadratic elements) with shift  $p = 900$ .



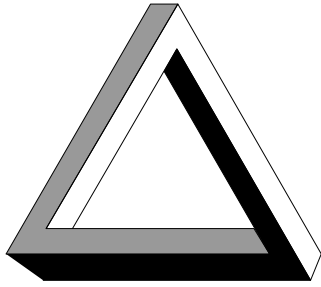
# *Eigenvectors*

What about the eigenvectors?

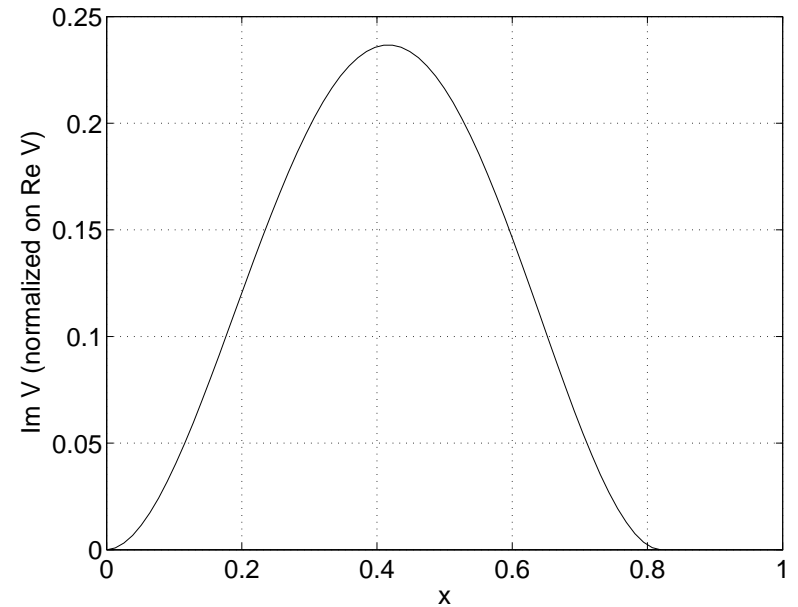
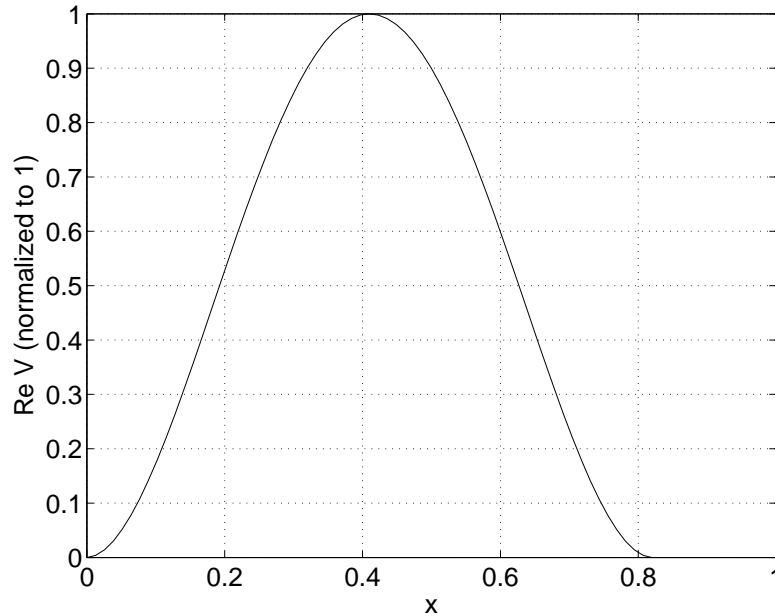
We are expecting to see...



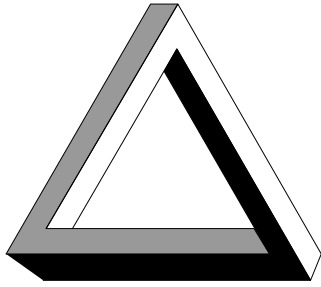
(centrifugal = real part, coriolis = imaginary part.)



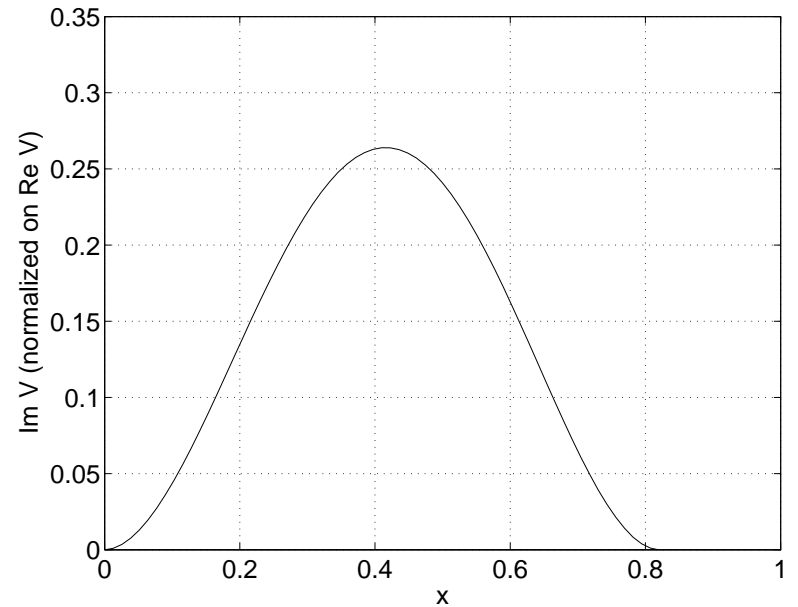
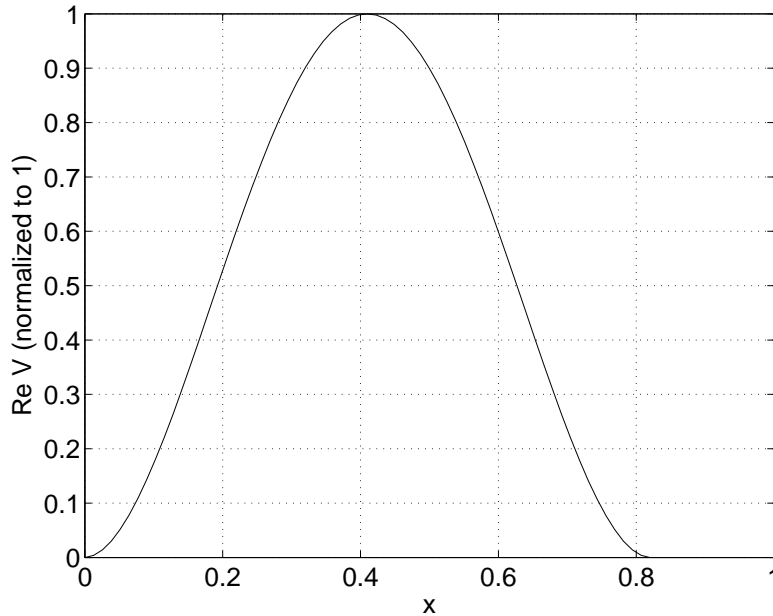
## *polyeig without shift*



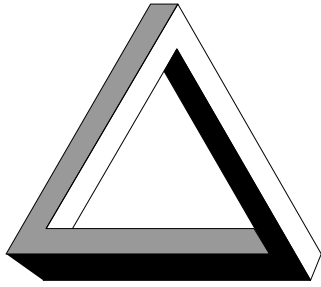
$\text{Re } V$  and  $\text{Im } V$  from Matlab's `eig` routine. No shift (32 elements).



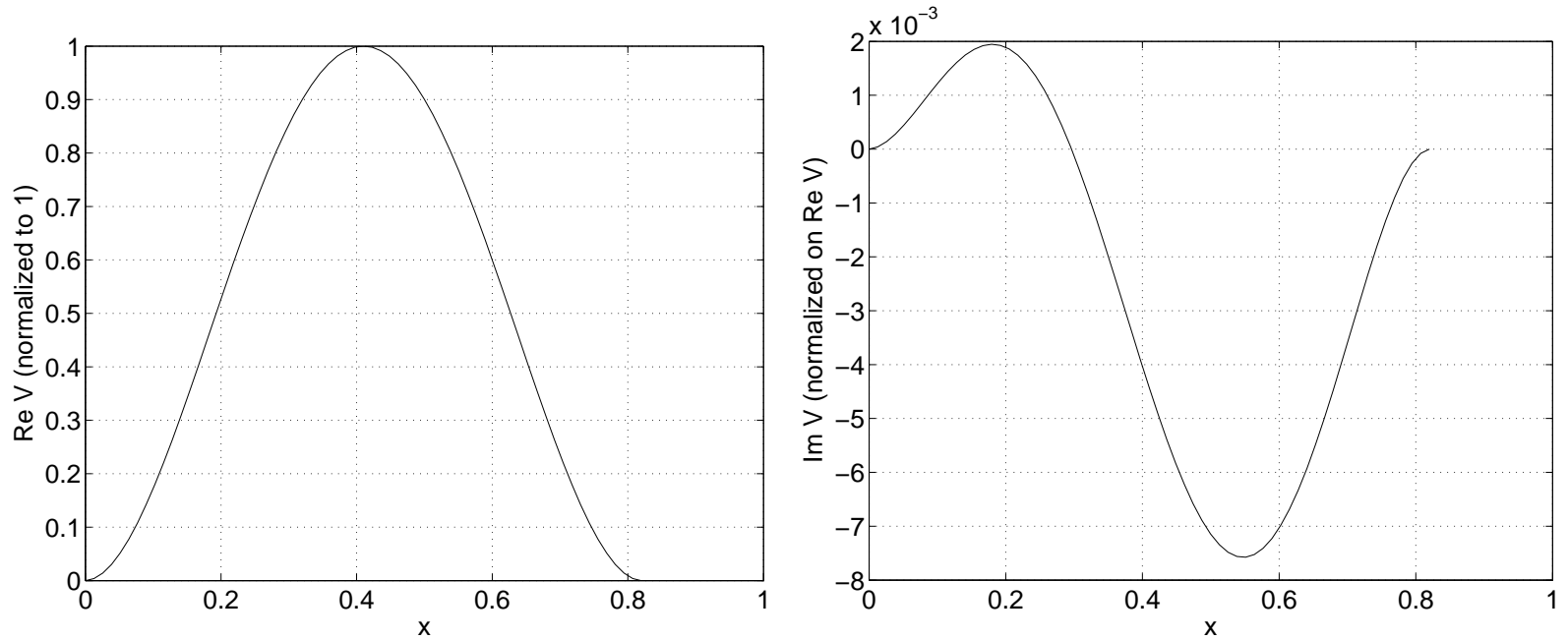
## *polyeig with shift*



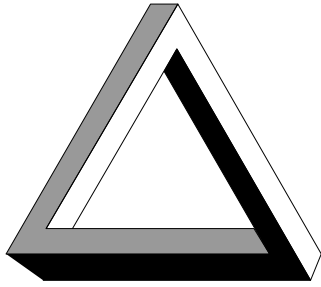
$\text{Re } V$  and  $\text{Im } V$  from Matlab's `eig` routine. Shift = 900 (32 elements).



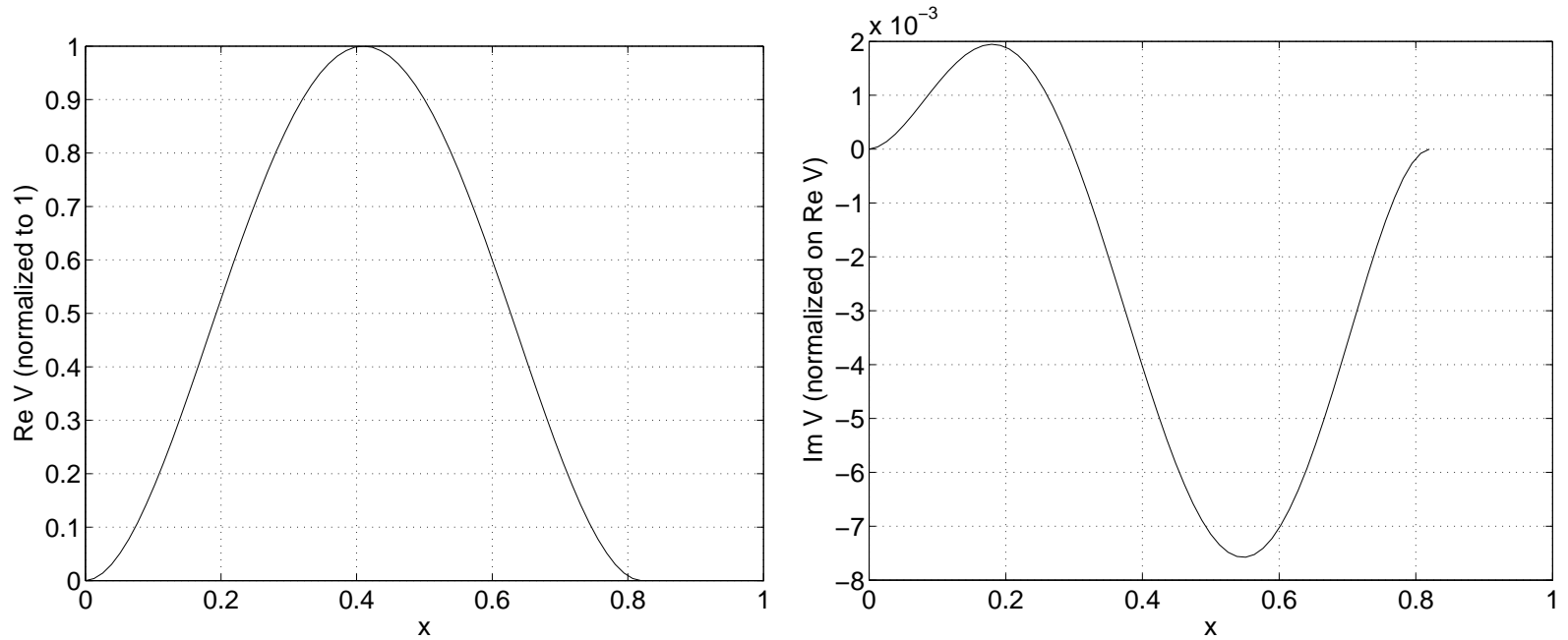
## *eig* without shift



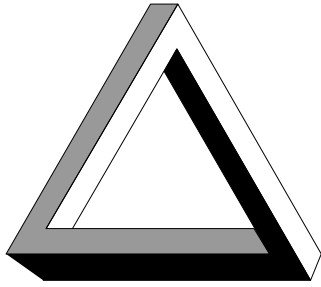
$\text{Re } V$  and  $\text{Im } V$  from Matlab's *eig* routine. No shift (32 elements).



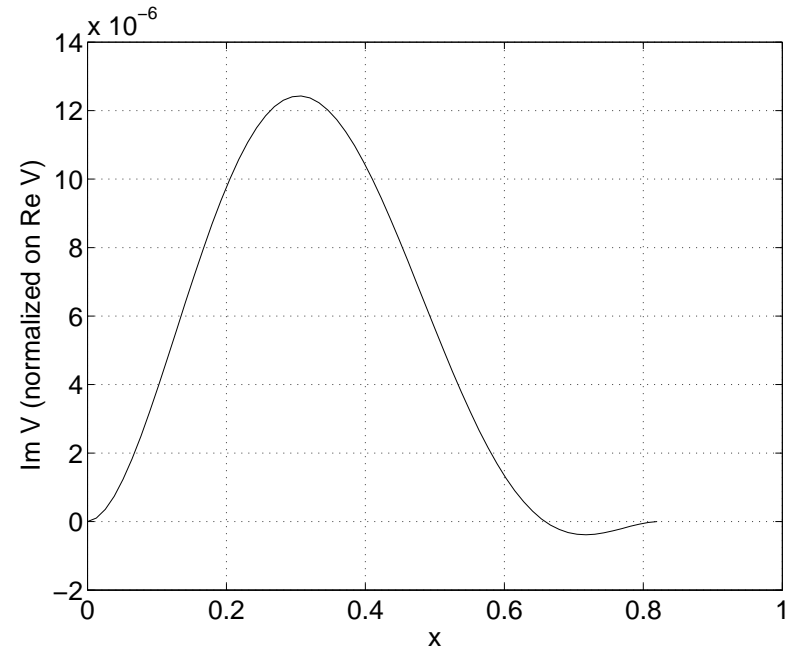
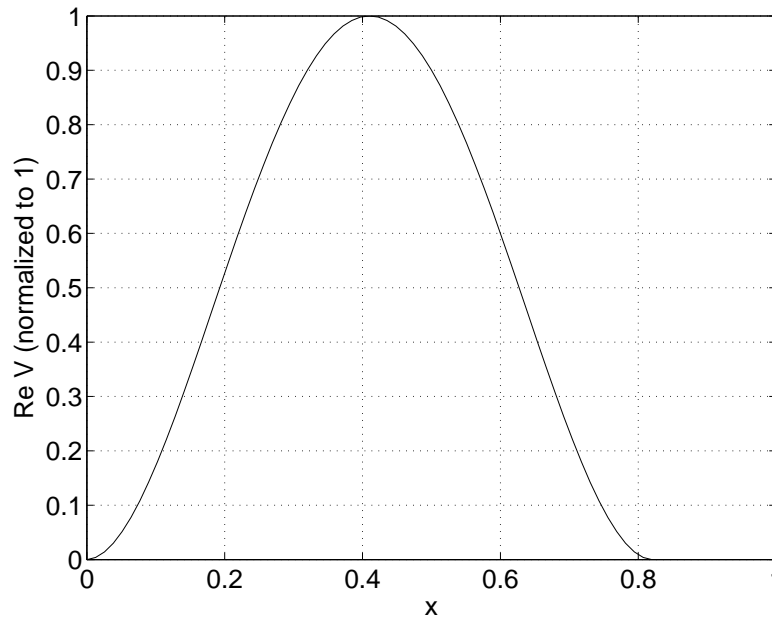
## *eig with shift*



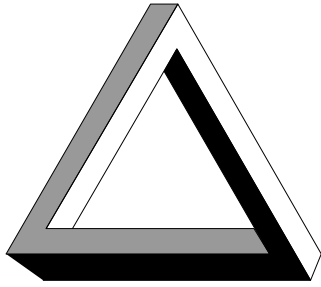
$\text{Re } V$  and  $\text{Im } V$  from Matlab's `eig` routine. Shift = 900 (32 elements).



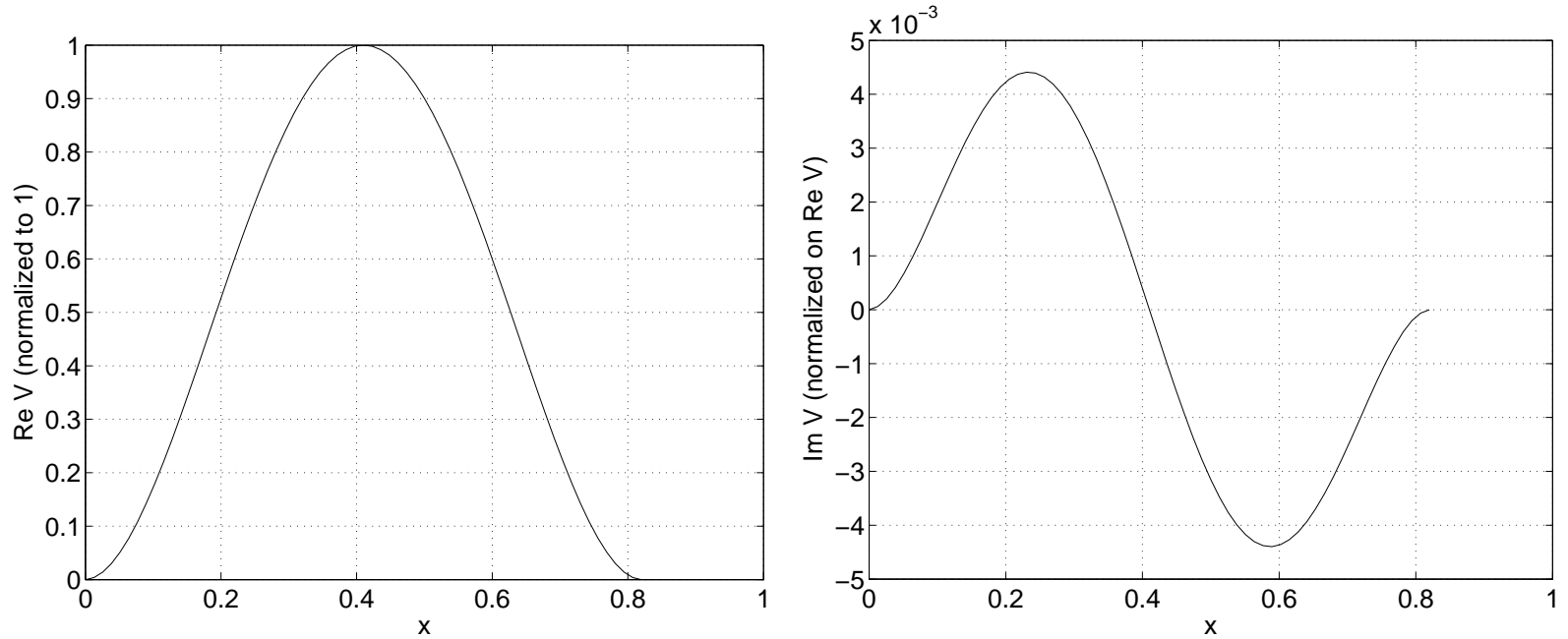
# *Inverse iteration without shift*



Re  $V$  and Im  $V$  from inverse iteration. No shift (32 elements).

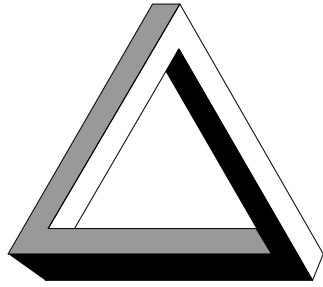


# *Inverse iteration with shift*



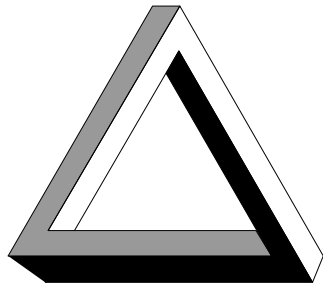
$\text{Re } V$  and  $\text{Im } V$  from inverse iteration. Shift = 900 (32 elements).





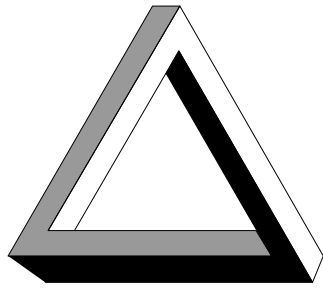
## Conclusion

- Shifted inverse iteration is most robust (given a good initial guess).
- ANSYS and matlab seem to struggle.
- Problem is due to rounding error (**a hunch!**)
  - $\omega^2 r$  and  $2\omega V$  are different orders of magnitude.
- A **challenge** for eigen-solvers?
- ...or is there an 'easy' remedy?



I'll leave you with the **fundamental inequality of applied mathematics**:

$$\|T - P\|_T \ll \|T - P\|_P$$

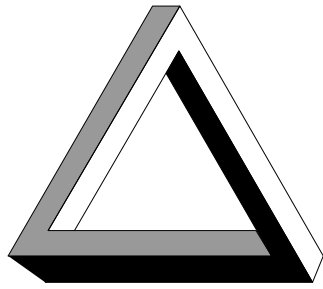


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$$\|T - P\|_T \ll \|T - P\|_P$$

*The difference between theory and practice in theory  
is less than  
the difference between theory and practice in practice.*

Anon, circa 20th Century



I'll leave you with the fundamental inequality of applied mathematics:

$$\|T - P\|_T \ll \|T - P\|_P$$

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Anon, circa 20th Century

**The End...**